MODELLING AND SIMULATION OF ELECTRIC VEHICLES

Part 1

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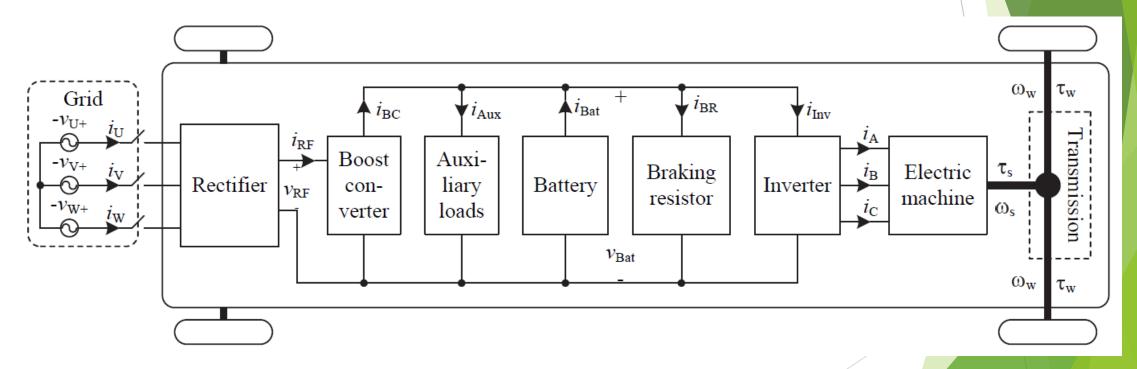
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Introduction

- ▶ Electric vehicles (EVs) are by many seen as the cars of the future as they are highly efficient, produce no local pollution, are silent, and can be used for power regulation by the grid operator.
- ► EVs still have critical issues which need to be solved. The three main challenges are limited driving range, long charging time, and high cost. These challenges are all related to the battery package of the car.
- In order to be able to estimate the energy consumption of the EV, and to test its features, it is very important to have a proper model (often called a digital twin) of the EV.
- ► The model of the EV is very complex as it contains many different components, e.g., transmission, electric machine, power electronics, and battery.

Vehicle modeling - architecture

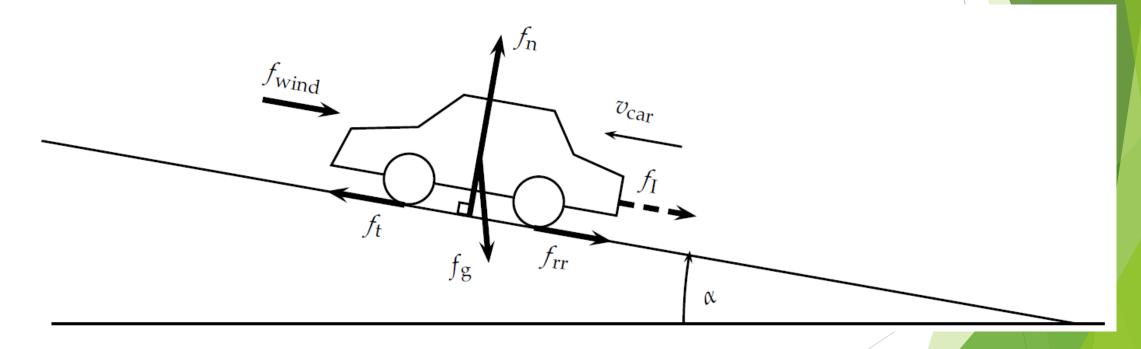
Many different architectures of the EV exist, as there are many possibilities, e.g., 1 to 4 electric machines, DC or AC machines, gearbox/no gearbox, high or low battery voltage, one or three phase charging, etc.



Example of architecture of the battery electric vehicle

Vehicle modeling - force model

► The forces which the electric machine of the vehicle must overcome are the forces due to gravity, wind, rolling resistance, and inertial effect.



Free body diagram of the forces (thick arrows) acting on the car

Vehicle modeling - force model

► The traction force of a vehicle can be described by the following two equations:

$$f_{t} = \underbrace{M_{\text{car}}\dot{v}_{\text{car}}}_{f_{\text{I}}} + \underbrace{M_{\text{car}}\cdot g \cdot \sin(\alpha) + \operatorname{sign}(v_{\text{car}})}_{f_{g}} \underbrace{M_{\text{car}}\cdot g \cdot \cos(\alpha) \cdot c_{\text{rr}}}_{f_{\text{rr}}} + \operatorname{sign}(v_{\text{car}} + v_{\text{wind}}) \underbrace{\frac{1}{2}\rho_{\text{air}}C_{\text{drag}}A_{\text{front}}(v_{\text{car}} + v_{\text{wind}})^{2}}_{f_{\text{wind}}}$$

$$(1)$$

$$c_{\rm rr} = 0.01 \left(1 + \frac{3.6}{100} v_{\rm car} \right), \tag{2}$$

Vehicle modeling - force model

where f_{t}	[N]	Traction force of the vehicle
$f_{ m I}$	[N]	Inertial force of the vehicle
$f_{ m rr}$	[N]	Rolling resistance force of the wheels
$f_{\mathbf{g}}$	[N]	Gravitational force of the vehicle
$f_{\rm n}$	[N]	Normal force of the vehicle
$f_{ m wind}$	[N]	Force due to wind resistance
α	[rad]	Angle of the driving surface
$M_{ m car}$	[kg]	Mass of the vehicle
$v_{\rm car}$	[m/s]	Velocity of the vehicle
$\dot{v}_{ m car}$	$[m/s^2]$	Acceleration of the vehicle
g = 9.81	$[m/s^2]$	Free fall acceleration
$\rho_{\rm air} = 1.2041$	$[kg/m^3]$	Air density of dry air at 20 °C
$c_{\rm rr}$		Tire rolling resistance coefficient
$C_{ m drag}$	[-]	Aerodynamic drag coefficient
$A_{ m front}$	$[m^2]$	Front area
$v_{ m wind}$	[m/s]	Headwind speed
Willia		

Vehicle modeling - auxiliary loads

A modern car have also other loads which the battery should supply. These loads are either due to safety, e.g., light, wipers, horn, etc. and/or comfort, e.g., radio, heating, air conditioning, etc.

Radio	52 W
Heating Ventilation Air Condition (HVAC)	489 W
Lights	316 W
Total p_{Aux}	857 W

Example of average power level of the auxiliary loads of the vehicle

Vehicle modeling - transmission

Torque, angular velocity, and power of the transmission system are given by the following equations:

$$\tau_{\rm t} = f_{\rm t} r_{\rm w} \tag{3}$$

$$\tau_{\rm W} = \frac{\tau_{\rm t}}{2} \tag{4}$$

$$\omega_{\rm W} = \frac{v_{\rm car}}{r_{\rm W}} \tag{5}$$

$$p_{\mathsf{t}} = f_{\mathsf{t}} v_{\mathsf{car}},\tag{6}$$

Vehicle modeling - transmission

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where \tau_{\rm t} [Nm] Traction torque \tau_{\rm w} [Nm] Torque of each driving wheel r_{\rm w} [m] Wheel radius \omega_{\rm w} [rad/s] Angular velocity of the wheels p_{\rm t} [W] Traction power
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$$\tau_{\rm s} = \begin{cases} \eta_{\rm TS} \frac{\tau_{\rm t}}{G}, p_{\rm t} < 0 \\ \frac{\tau_{\rm t}}{\eta_{\rm TS} G}, p_{\rm t} \ge 0 \end{cases}$$

(8)

(9)

$$\omega_{\rm s} = G\omega_{\rm w}$$

$$p_{\rm s}=\tau_{\rm s}\omega_{\rm s}$$
,

where τ_s [Nm] Shaft torque of electric machine ω_s [rad/s] Shaft angular velocity of electric machine p_s [W] Shaft power of electric machine G [-] Gear ratio of differential

- For propulsion usually the induction machine (IM), permanent magnet synchronous machine (PMSM), and switched reluctance machine (SRM) are considered.
- The "best" choice is like many other components a trade off between cost, mass, volume, efficiency, reliability, maintenance, etc.
- Due to its high power density and high efficiency, the PMSM is selected as an example.
- The electric machine is divided into an electric part and mechanic part.
- ► The electric part of the PMSM is modeled in the DQ-frame:

$$v_{\rm d} = R_{\rm s}i_{\rm d} + L_{\rm d}\frac{di_{\rm d}}{dt} - \omega_e L_{\rm q}i_{\rm q} \tag{10}$$

$$v_{q} = R_{s}i_{q} + L_{q}\frac{di_{q}}{dt} + \omega_{e}L_{d}i_{d} + \omega_{e}\lambda_{pm}$$
(11)

$$p_{\rm EM} = \frac{3}{2} \left(v_{\rm d} i_{\rm d} + v_{\rm q} i_{\rm q} \right),$$
 (12)

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where v_{\rm d}
                          D-axis voltage
                          Q-axis voltage
         i_{\rm d}
                          D-axis current
         \frac{i_{\mathrm{q}}}{R_{\mathrm{s}}}
                   A
                          Q-axis current
                          Stator phase resistance
                   \Omega
                          D-axis inductance
                   [H]
                   [H]
                          Q-axis inductance
                 [Wb]
                          Permanent magnet flux linkage
         \lambda_{\rm pm}
                [rad/s] Angular frequency of the stator
         \omega_{
m e}
                        Permanent magnet flux linkage
         \lambda_{\rm pm}
                          Electric input power
         p_{\rm EM}
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The mechanical part of the PMSM can be modeled as follows:

$$\tau_{\rm e} = J_{\rm s} \frac{d\omega_{\rm s}}{dt} + B_{\rm v}\omega_{\rm s} + \tau_{\rm c} + \tau_{\rm s} \tag{13}$$

$$p_{\rm s} = \tau_{\rm s}\omega_{\rm s},\tag{14}$$

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where J_s [kgm<sup>2</sup>] Shaft moment of inertia \tau_e [Nm] Electromechanical torque \tau_c [Nm] Coulomb torque B_v [Nms/rad] Viscous friction coefficient
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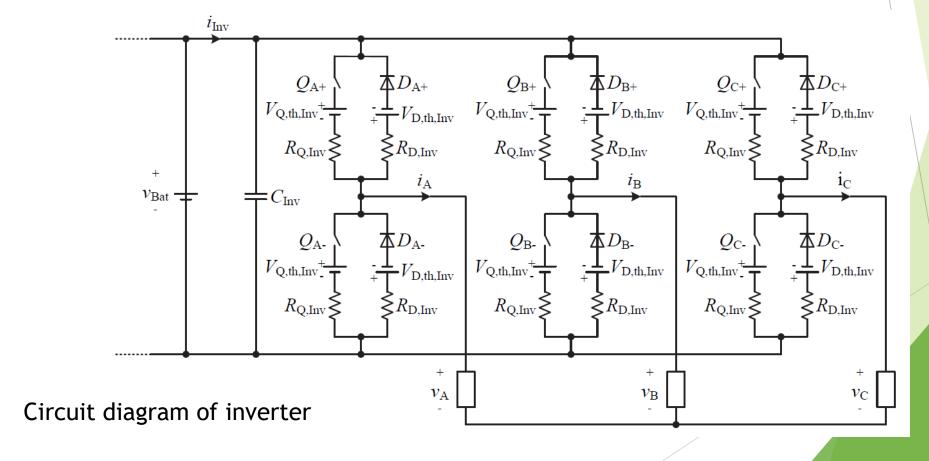
► The coupling between the electric and mechanic part is given by:

$$\tau_{\rm e} = \frac{3}{2} \frac{P}{2} \left(\lambda_{pm} i_{\rm q} + \left(L_{\rm d} - L_{\rm q} \right) i_{\rm d} i_{\rm q} \right) \tag{15}$$

$$\omega_{\rm e} = \frac{P}{2}\omega_{\rm s},\tag{16}$$

where P [-] Number of poles

The inverter transmits power between the electric machine (with phase voltages vA, vB, and vC) and the battery by turning on and off the switches QA+, QA-, QB+, QB-, QC+, and QC-.



▶ The average power losses of one switch pQ, Inv and diode pD, Inv during one fundamental period are:

$$p_{Q,Inv} = \left(\frac{1}{8} + \frac{m_{i}}{3\pi}\right) R_{Q,Inv} \hat{I}_{p}^{2} + \left(\frac{1}{2\pi} + \frac{m_{i}}{8} \cos(\phi_{EM})\right) V_{Q,th,Inv} \hat{I}_{p}$$
(17)

$$p_{\rm D,Inv} = \left(\frac{1}{8} - \frac{m_{\rm i}}{3\pi}\right) R_{\rm D,Inv} \hat{I}_{\rm p}^2 + \left(\frac{1}{2\pi} - \frac{m_{\rm i}}{8} \cos(\phi_{\rm EM})\right) V_{\rm D,th,Inv} \hat{I}_{\rm p}$$
(18)

$$m_{\rm i} = \frac{2\hat{V}_{\rm p}}{V_{\rm Bat}},\tag{19}$$

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where p_{Q,Inv}
                      [W] Power loss of one switch
                      [W] Power loss of one diode
         p_{\rm D,Inv}
                     [rad] Power factor angle
         \phi_{\mathrm{EM}}
                      [A] Peak phase current
                           Peak phase voltage
                           Modulation index
         m_{\rm i}
         V_{\mathsf{Bat}}
                           Battery voltage
                           Inverter switch resistance
         R_{Q,Inv}
                           Inverter diode resistance
         R_{\rm D,Inv}
                      \Omega
                           Inverter switch threshold voltage
         V_{\rm Q,th,Inv}
                           Inverter diode threshold voltage
         V_{\mathsf{D},\mathsf{th},\mathsf{Inv}}
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The total power loss of the inverter is given by:

$$P_{\text{Inv,loss}} = 6 \left(P_{\text{Q,Inv}} + P_{\text{D,Inv}} \right) = \frac{3}{2} R_{\text{Inv}} \hat{I}_{\text{p}}^2 + \frac{6}{\pi} V_{\text{th,Inv}} \hat{I}_{\text{p}}.$$

► The inverter input power and efficiency are:

$$p_{\text{Inv}} = v_{\text{Bat}} i_{\text{Inv}} = p_{\text{EM}} + p_{\text{Inv,loss}}$$

$$\eta_{\text{Inv}} = \begin{cases} \frac{p_{\text{EM}}}{p_{\text{Inv}}}, p_{\text{EM}} \geq 0 \\ \frac{p_{\text{Inv}}}{p_{\text{EM}}}, p_{\text{EM}} < 0, \end{cases}$$

where i_{Inv} [A] Inverter input current p_{Inv} [W] Inverter input power η_{Inv} [-] Inverter efficiency

(20)

(21)

(22)

Vehicle modeling - battery

- The battery pack is the heart of an electric vehicle.
- Many different battery types exist, e.g., lead-acid, nickel-metal hydride, lithium-ion, etc.
- Today, the lithium-ion is the preferred choice due to its relatively high specific energy and power.
- As an example, the battery model will be based on a Saft VL 37570 lithium-ion cell.
- ▶ Both electric and capacity battery models will be presented.

Vehicle modeling - battery

Maximum voltage	$V_{ m Bat,max,cell}$	4.2 V
Nominal voltage	$V_{ m Bat,nom,cell}$	3.7 V
Minimum voltage	$V_{ m Bat,min,cell}$	2.5 V
1 h capacity	$Q_{1,\text{cell}}$	7 Ah
Nominal 1h discharge current	$I_{ m Bat,1,cell}$	7 A
Maximum pulse discharge current	$I_{\text{Bat,max,cell}}$	28 A

Data sheet specifications of Saft VL 37570 Li-lon battery